

Frequency response of transformer winding to investigate the influence of RLC

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ABSTRACT

Frequency response measurements are used for power transformer winding failures detection. The variation between frequency responses indicate mechanical changes in the transformer winding. One method to investigate winding failures in transformer is to develop a reliable circuit model which can simulate the frequency response of an actual winding. The main reason to use the model is because it is expensive to create damages on an actual winding. This paper proposes n-stages circuit ladder network to simulate the response of a winding which has unique design. It presents a new technique to calculate the resistance, inductance and capacitance of the winding. Then, the relationship between the RLC parameters and the frequency response is studied. The winding chosen in this investigation is a single phase 33kV transformer winding. The simulated frequency response was compared with the measured response to verify the proposed model. The model can give a comprehensive understanding about the effect of RLC parameters on the frequency response.

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1. INTRODUCTION

Power transformers are designed to provide safe, reliable delivery of electricity to the public and consumers. However, operating the transformer at very high loading condition to meet the demands can accelerate the deterioration of the unit. This is due to the increase of mechanical, electric, and thermal stresses during the operation. If the transformer insulation conditions degraded, the clamping pressure could become loose thus other failures accrued. This would reduce the ability of a transformer to withstand high current from short circuit fault. In addition, there are other failures that could occur such as mishandling the unit during transportation, earthquakes and even combustible gas explosion [1]. For his reason, it is important to conduct studies to investigate the transformer failures.

Today, the FRA has become a complementary technique in order to investigate the transformer failures. The FRA measurement typically performs at a frequency range (50Hz to 5MHz) [1]. Based on IEEE [2] standard and CIGRE [3] it is approximately in the range of 20Hz to 2MHz. The FRA test is used to detect mechanical deformation in a transformer. It is applied after some incidents that have the possibility of causing this mechanical or electrical damage to the power transformer. Physical changes in the resistance, inductance and capacitance network of the transformer windings can alter the mathematical transfer function. The transfer function behavior can detect a wide range of mechanical or electrical changes in the electrical

circuit representation of the transformer. Besides mechanical damage, FRA is also sensitive to dielectric changes such as due to aging which is not categorized as a mechanical fault [4].

In order to investigate the effect of winding failures on FRA measurement, faults need to be applied in the actual winding. However, this is difficult and costly because of the transformer winding strength and the price of transformer. For this reason, it is more practical to perform winding failures in a transformer model represented using suitable software. It is known that transformer winding can be represented by electrical circuit with parameters of resistance, inductance, and capacitance (RLC). Therefore, it is important to be accurate in calculating winding parameters. There are various techniques used to simulate the transformer RLC model such as finite element method (FEM) and state space model. A study conducted in [5] used finite element analysis to calculate the inductance and capacitance of the winding in order to investigate the winding deformation. It was founded that FEM gives an accuracy in acceptable limits. Also, a study conducted in [6] to study a radial deformation in the winding using FEM. It was shown that FEM can provides a significant information about the changes of capacitance and inductance of the winding. The weakness in FEM is that it obtains only approximate solution. In addition, it was stated in [7] that FEM has an inherent error. On the other hand, a state space modeling was presented in [8] to simulate the actual measurement distribution transformer. It was founded that it is easy to realize the impact of various mechanical deformations on the transformer FRA signature.

In this paper, a lumped ladder network model is presented. The advantages of the model are that the physical meaning of the model parameters is easy to identify. This model can be used later to simulate various winding damages. For example, it is easy to identify the disc required to apply the fault in. In addition, it is more physical to make the changes. The novelty in this study is that the winding structure itself is entirely new thus poses new challenges that requires different approach to simulate the frequency response.

This study presents a lumped parameter equivalent circuit model which represent actual HV winding. The winding geometry was taken from an actual transformer HV winding. Then, the RLC parameters were calculated using a new method for the new winding structure. The simulated response shows an approximately similar when compared with the measured response. Then, changes in the RLC parameters are applied to investigate the effect on the response. This model can also be used to investigate the effect of number of discs on the response. Nevertheless, the main purpose of this study is to investigate the relationship between the level of fault-based on the change of winding resistance, capacitance and inductance.

2. HIGH-FREQUENCY MODELING OF TRANSFORMERS

Modeling the high frequency response of transformer winding has a certain degree of complexity. This is due to the arrangement of transformer winding electrical circuit. It is impossible to use a simple equivalent circuit to present the transformer winding. This is because at higher frequencies wavelength of the signals are compared with the transformer winding geometry [9].

The steps shown in Figure 1 are followed for calculating the high frequency response of transformer winding. The first step is to measure the winding geometry. The second step is to calculate the winding resistance, capacitance, self and mutual inductance using certain formulas. Then, the calculated resistance, series capacitance, self and mutual inductance are entered in MATLAB to calculate the frequency response.

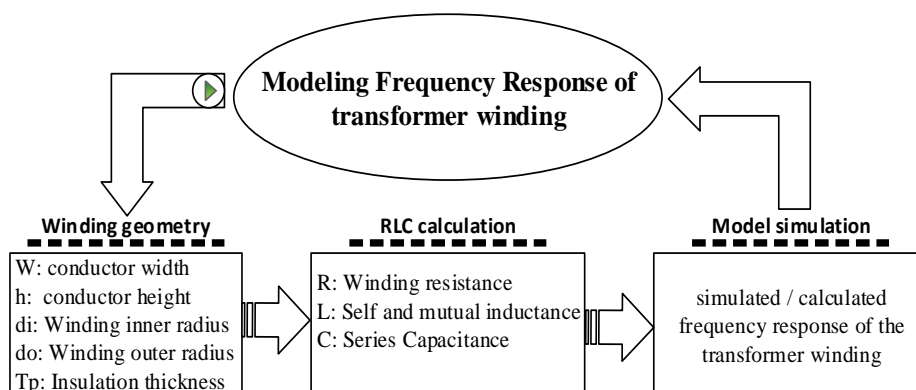


Figure 1. The modeling steps to calculate the frequency response of transformer winding

2.1. N-Ladder Network

As shown in Figure 2(a) n-stage of ladder network method is a well-known method to model the transformer winding. Each disc of the winding is represented by resistance, capacitance, and inductance. In every disc, for example $D1$ shown in Figure 2(a) consists of series inductance L_s , series capacitance C_s , series resistance R_s and ground capacitance C_g .

First step the winding geometry was measured manually such as conductor geometry and winding inner and outer radius. The transformer was approximately looked like Figure 2(b). According to [10], there are several types of transformer winding and have different ways of calculation. The main types of the winding are helical winding, layer winding, and disc winding. The transformer selected in this study is disc winding. The equivalent circuit of the disc winding transformer for n-stage ladder network is shown in Figure 2

Figure 2(a), in order to simulate the transformer winding frequency response, it is required to calculate the total series capacitance C_s . This required to calculate the capacitance in between turns C_t for every disc. In the meantime, it is essential to calculate the capacitance in between discs C_d . After that, calculate the series resistance R_s , capacitance to the ground C_g , conductance G_s , self and mutual inductance M_L . Those electrical parameters must be obtained as a second step to simulate the frequency response of the transformer winding.

2.2. Series Capacitance Calculation

Based on the transformer winding structure as shown in Figure 2(b), the capacitance between the conductors in the same disc C_t needs to be calculated in order to find the series capacitance. At the same time, the capacitance between conductors in the adjacent disc C_d (capacitance between discs) is also calculated. The capacitance between two conductors represents C_t is shown in Figure 3. The capacitance between two turns is given by (1).

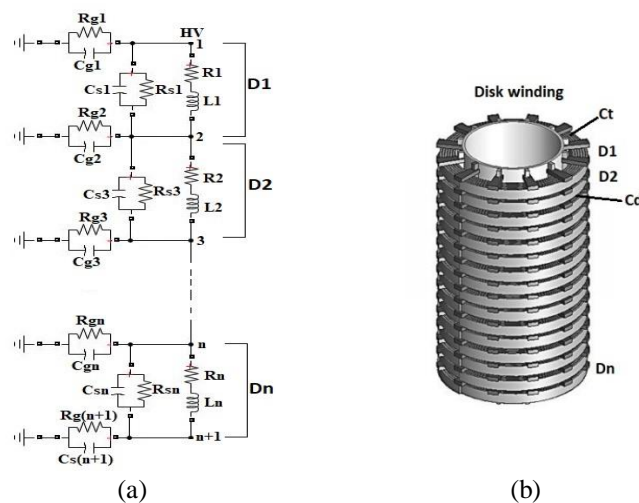


Figure 2. (a) N-stage equivalent lumped circuit for the single winding, (b) the 3D of single-phase winding [11]

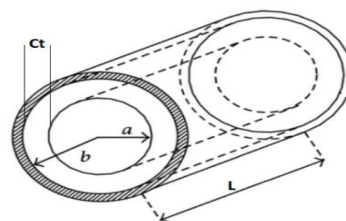


Figure 3. The two conductors diagram soiled line the first conductor dotted line the second conductor [12]

Where the L is the length of the conductor which represent the height. b and a are the inner radius and outer radius of the outer and inner conductors respectively. ϵ_o is permittivity of the free space which is

8.854×10^{-12} and ϵ_r is 3.85 which is the relative permittivity of the insulation paper located between the outer and inner conductors. On the other hand, the capacitance between adjacent discs as in Figure 4 can be calculated by (5) which derived as shown in (2), (3) and (4).

$$C_t = \frac{2\pi\epsilon_r\epsilon_0 L}{\ln \frac{b}{a}} \quad (1)$$

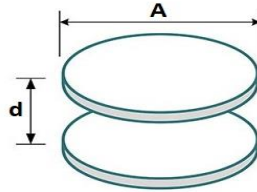


Figure 4. The capacitance in between two discs

$$C_d = \frac{\epsilon(A)}{d} \quad (2)$$

$$A = \pi(r_o^2 - r_i^2) \quad (3)$$

$$A = \pi \left(\frac{d_o^2}{4} - \frac{d_i^2}{4} \right) \quad (4)$$

Where: $\epsilon = \epsilon_r \epsilon_0$

$$C_d = \epsilon_r \epsilon_0 \pi \times \frac{d_o'^2 - d_i'^2}{4 \times d} \quad (5)$$

Where: $d_o' = d_o + d$
 $d_i' = d_i - d$

d is the distance between turns (accounting for fringing effect). d_i and d_o are the inner and outer diameter if the winding. Figure 5 is an example of an equivalent network of two discs in the winding. The circuit shows that C_t is contacted in series whereas the C_d are in parallel. Since C_t for every between two conductors are different due to different conductor length, therefore we calculate all C_t and the total is considered in series as (6).

$$C_{t \text{ total}} = \frac{1}{\frac{1}{C_{t1}} + \frac{1}{C_{t2}} + \frac{1}{C_{tn}}} \quad (6)$$

On the other hand, the total capacitance between discs is given as (7).

$$C_{d \text{ total}} = C_{d1} + C_{d2} + C_{dn} \quad (7)$$

Since the capacitance in between discs is in parallel as shown in the equivalent circuit Figure 5. The total series capacitance of whole winding can be calculated as (8). However, for a one disc the total series capacitance can be obtain by $C_d + C_t$. Regarding to this particular winding in this study the in (8) can give the most similar response compared with the measured response [13], [14].

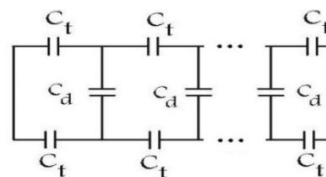


Figure 5. Layout of the equivalent capacitance diagram network of the winding

$$C_s = \frac{1}{Nd} \left(\frac{C_t}{mt} + 4C_{dt} \right)$$

$$C_{dt} = \frac{(mt-1)(2mt-1)}{6mt} C_d \quad (8)$$

Where the C_{dt} is the resultant inter-disc capacitance. In addition, there is also capacitance to the ground C_g . In this study, the measured transformer winding do not have capacitance to the ground since there is no grounded tank during the measurement. There are other electrical parameters to be calculated in order to simulate the response such series resistance R_s , self, and mutual inductance.

2.3. The Series Resistance Calculation

To calculate the series resistance of the winding, it is required to know the total circumference of the conductor C_{ir} . The total circumference is given in $C_{ir} = 2\pi r$.

$$R_s = R_{s1} \times C_{ir} \quad (9)$$

$$R_{s1} = \frac{1}{2(h+w)} \sqrt{\frac{\pi f \mu}{\sigma}} \Omega/\text{m} \quad (10)$$

From (10), h , w , are the height and width of the conductor respectively. Where f is the signal frequency, μ and σ are the permeability and conductivity of the conductor. On the other hand, the conductance G is a matrix which can be obtained from (11) where $\tan\delta$ is the insulation dissipation factor.

$$G = 2\pi f C_s \tan\delta \quad (11)$$

2.4. The self and Mutual Inductance Calculation

The self and mutual inductance between turns were obtained from (12), (13).

$$L_{km} = \mu_0 N_k N_m \sqrt{(r\alpha)} \frac{2}{k} \left[\left(1 - \frac{k^2}{2} \right) K(k) - E(k) \right] \quad (12)$$

$$K = \sqrt{\frac{4\alpha r}{z^2 + (\alpha + r)^2}} \quad (13)$$

Where L_{km} is the mutual inductance between disc k and disc m . r is the average radius of the discs and z is the axial distance between the two discs. N_k and N_m are the number of turns in k -th section and m -th section as shown in Figure 6. K and E are the elliptic integrals of the first and second kinds. For self-inductance where: $k = m$, z is calculated by $z = 0.2235 \times (h+w)$. Also, h_1 and w_1 are alike to h_2 and w_2 . The self inductance for the L_{km} matrix is representing the diagonal elements while off-diagonal elements are the mutual inductance between discs. In this study, the value of r and α are equaled. This is because the average radius of the sections are the same. The value of magnetic permeability of the medium is $\mu_0 = 4\pi \times 10^{-7}$.

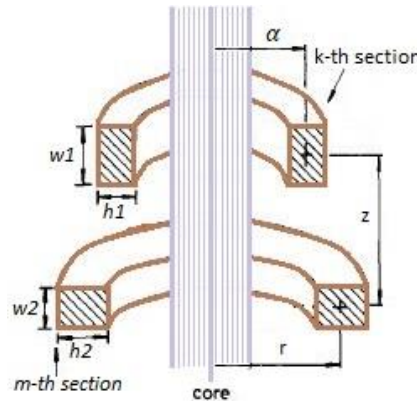


Figure 6. The general dimensions of the winding discs

3. RESULTS AND ANALYSIS

3.1. Measurement of the Actual Transformer

The measurement was conducted on an actual transformer in order to verify and compare with the developed model. FRA measurement was performed on the HV winding. Also, it is performed from 20Hz to 2MHz. The transfer function obtained by the ratio V_{out}/V_{in} based on CIGRE reported in [3]. The measurement configuration is taken in single phase HV winding as shown in Figure 7. This measurement configuration is mostly used because it provide enough information to analysis the transformer condition.

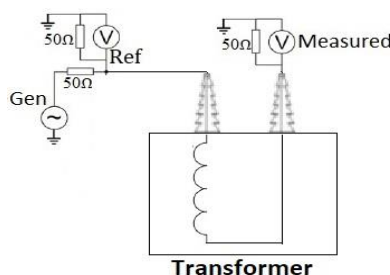


Figure 7. FRA measurement test configuration

3.2. Parameters Calculation on the Measured Transformer

The FRA measurement is conducted on a single phase 33kV HV winding. To calculate electrical parameters of the tested transformer, the specifications of the geometrical such as dimension of the conductor and thickness of the insulation are calculated. The full winding consists of 96 discs. In every disc, there are five turns. In every turns there are six conductors connected together at the terminal. This is the novelty in this paper where a new winding design is studied to calculate its electrical parameters and simulate the frequency response.

The full winding structure is shown in Figure 8. The conductor has 2.4mm width and 11.5mm in height as shown in Figure 9(b). Based on Table 1 the transformer dimensions such inner and outer radius were calculated. The total circumference of the conductor is given by $2\pi r$. The winding parameters are provided in Table 1. The insulation thickness between conductors is 0.5mm. However, there is an air gap between turn 3 and turn 4. The 5mm air gap is shown in Figure 9(a).

As given in Table 1 the winding dimensions such as inner and outer radius were calculated. The total circumference of the conductor is given by $2\pi r$. Based on winding parameters provided in Table 1, capacitance, resistance and inductances are calculated.

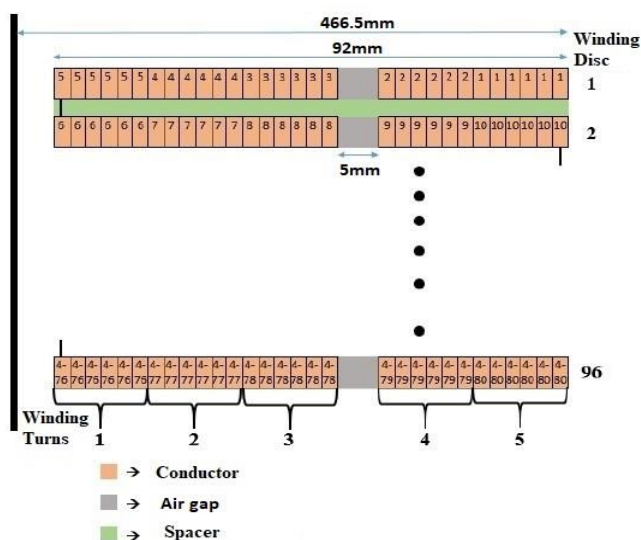


Figure 8. The 2D for the full winding structure tested transformer

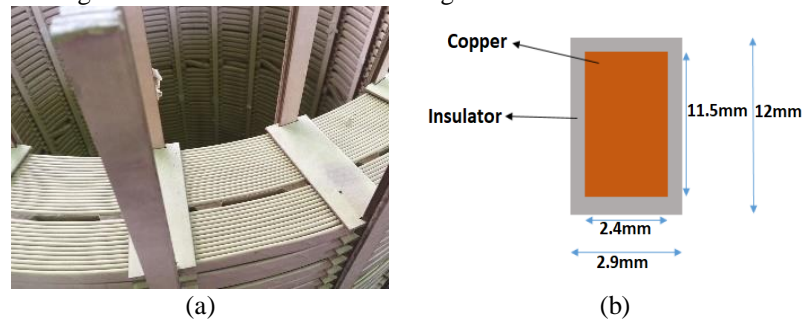


Figure 9. (a) the transformer winding structure with 5mm of air gap between particular turns, (b) the conductor measurement dimensions

Table 1. The Transformer Parameters Specifications

Winding Geometry in mm	
Conductor width (W)	2.4
Conductor high (h)	11.5
Insulation thickness t_p	0.5
Number of turns per disc (mt)	30
Air gap insulation thickness	5
Pressboard thickness between discs d	3
Winding inner radius r	374.5
Outer diameter do	933
Inner diameter di	749
The total circumference of the conductor C_{ir}	94238.64

3.3. Comparison between the Measurement and Simulation

The model is applied to simulate the frequency response of the continuous disc winding. Figure 10 shows the measured and the simulated responses of the HV winding. The dashed line presents the measured response while the solid line is the simulated response. The two responses show the same path of negative and positive slope. Nonetheless, there are some differences in the resonance at the high-frequency region. These resonances are not shown in the calculated response. It is believed that this is because 5mm air gap only included in series capacitance and self inductance calculation. However, it is required to included in mutual inductance calculation. The same transformer is recommended to be studied in the future and calculate the mutual inductance with the air gap effect.

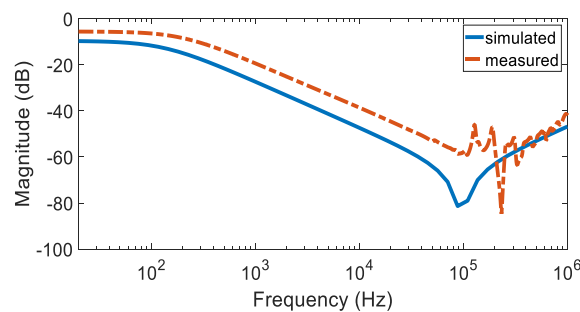


Figure 10. The calculated vs. measured responses for the HV winding of 96 discs winding

However, Figure 11 shows the measured and simulated responses of the same winding after improvement. The simulated response shows more similar to the measured response. This is because of some changes in the winding resistance R_s , conductance G_s , and self-inductance. This improvement is implemented using trial and error method. The changes are applied by decreasing winding resistance, conductance, and self-inductance. The total results of the transformer winding electrical parameters are provided in Table 2. It also includes parameters of the improved simulated response. To further understand

the results shown in Table 2, more investigation is needed on the chosen transformer winding structure and the calculation of its electrical parameters. This future recommendation is to explain the reason of minor different between simulation and measured responses. Even though, the assumed spacing are air gap. But in actual transformer it includes press board and oil partials which is believed makes the differences in simulated and measured responses.

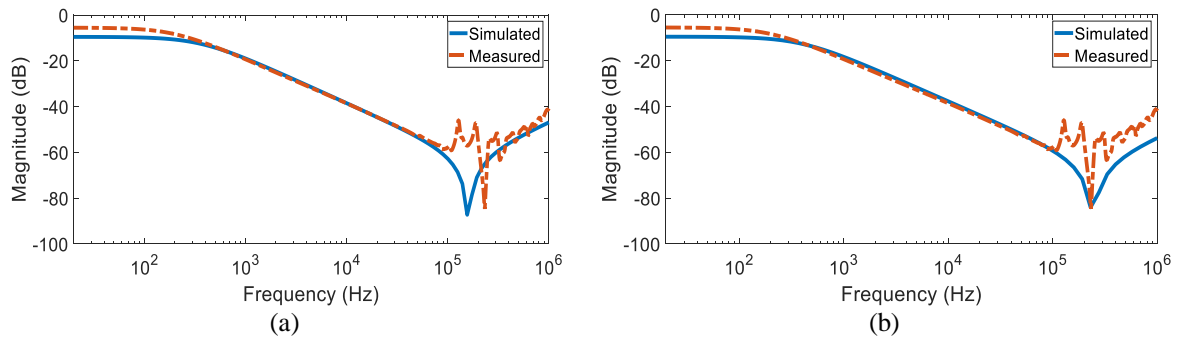


Figure 11. The Adjusted calculated vs. measured response (a) presents first improved results (b) presents the second improved results

Table 2. The Total Results of the Transformer Model Electrical Parameters Calculation

Parameters	Calculated response	Response	Response
		in Figure 11(a)	in Figure 11(b)
C_r	$3.18 \times 10^{-11} \text{F}$	-	-
C_d	$2.79 \times 10^{-9} \text{F}$	-	-
C_{shv}	$2.82 \times 10^{-9} \text{F}$	-	-
G_{shv}	$3.55 \times 10^{-9} \Omega$	$3.55 \times 10^{-12} \Omega$	-
R_{shv}	0.8806Ω	$0.88 \times 10^{-9} \Omega$	$1 \times 10^{-3} \Omega$
MR	Matrix 96×96	-	-
ML	Matrix 96×96	ML/100	ML/3
C_g	0F	-	-

3.4. RLC Analysis

Based on the obtained results, it can be realized that the frequency response is affected by the change of winding R , L and C values. The changes in electrical parameters cause the frequency response to shift towards lower or higher frequency. To investigate the sensitivity of the model and simulate winding faults, the following changes are applied:

- Increase of series capacitance C_s as shown in Figure 12.
- Increase of series resistance R_s as shown in Figure 13.
- Increase of self-inductance L_s as shown in Figure 14.

By increasing the winding capacitance, the response is shifted towards low frequency. The simulated response in Figure 12 represent the winding when it has high capacitance which is ten times higher than the normal winding response. By referring to Table 3 which is taken from other literature, the increase of series capacitance is mainly due to the aging of transformer insulation. Table 3 shows the investigated parameters that influence the frequency response.

On the other hand, the increase of series resistance is affecting the response at low frequency as shown in Figure 13. In the figure, the simulated response at frequencies below 10kHz showed a drop in magnitude. The increase of resistance is usually due to damages such as in the tap changer according to Table 3. Based on a study on tap changer damage in [15], findings in the reference also shows a similar effect on the measured response which refers to a coking in the tap changer.

The increase of self-inductance by ten times of the original value has a significant change in the simulated response. The anti-resonance which was originally at 200kHz has been shifted towards low frequency at 30kHz and showed a drop in magnitude on the negative slope. Such changes on the response is believed to be due to short circuit and core deformation as mentioned in Table 3.

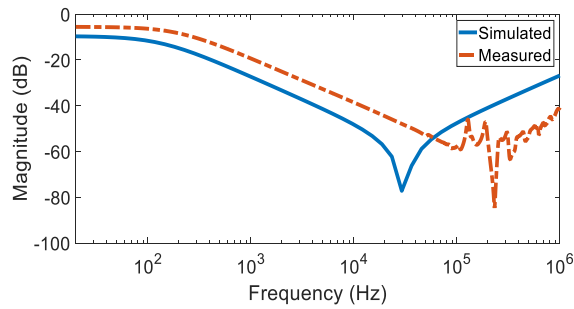


Figure 12. Increasing of series capacitance by 10 times ($C_{shv} \times 10$)

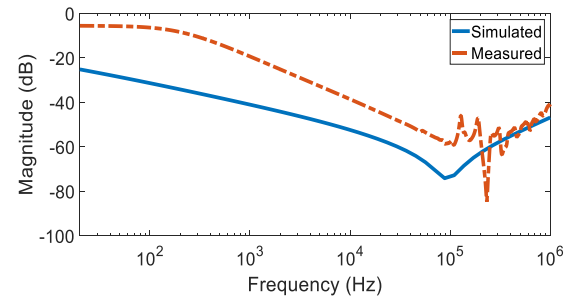


Figure 13. Increasing the series resistance by 10^3

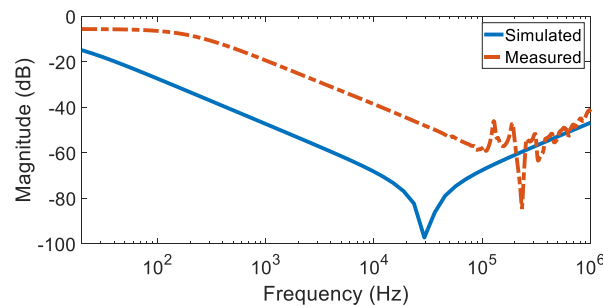


Figure 14. The changes in self-inductance which increased 10 times ($M_L \times 10$)

Table 3. Model Parameters and the Transformer Faults Which Influence [16]

Model parameter	Type of fault
Series capacitance, C_s	Aging of insulation, moisture content ingress and disk movement (displacement)
Resistance, R_s	Short or broken disk, failure of caulking contacts, tap changer damage.
Inductance, L_s	Disk deformation, local breakdown, core deformation winding short circuit.

4. CONCLUSION

It has been noted that FRA is a reliable method to investigate the mechanical condition of transformer winding. This paper presents a study on a unique transformer winding structure to simulate the frequency response. This winding has 5mm air gap in between winding turns 2 and 3 thus present a challenge to simulate the response as the winding turns are not uniformly distributed. In this study, we present a new technique which is to calculate the capacitance in between turns C_t separately. Similarly goes with the calculation of capacitance between discs, C_d . In addition, the self-inductance per disc considered in this study is that there are actually two different self-inductances which are connected in series. This is due to the insulation gap in between turns 2 and 3. It has been observed that increasing the series capacitance causes shifting in the response towards low frequencies. Whilst increasing the winding resistance shows a drop in magnitude at the low-frequency region. In fact, the change in self-inductance shows a major effect on the response. The response shows a drop in the anti-resonance of the response. In the meantime, the drop in response is clearly shown at low frequencies. In this paper, RLC analysis only investigate the increasing of series capacitance, series resistance, and self-inductance. This is because we believed that these three parameters have major effect on the frequency response. Further study is recommended to develop state space model for this particular transformer which could be compare with the proposed model. This is to conclude which approaches can give similar to the measured response. But, it is believed that the minor changes between simulation and measured responses is because of the assumptions of the winding spaces. The spaces includes a wooden press board and oil partials which has an effect on the frequency response.

SYMBOLS

N_d	Number of discs
m_t	Number of turns per disc
d	The distance between two discs
h	Height of the turns without insulation.
w	Width of the turns without the insulation.
C_{ir}	The total circumference of the conductor.
ϵ_o	The permittivity of free space
ϵ_r	Relative permittivity of the insulation paper
C_t	The capacitance in between turns
C_d	Capacitance in between the discs


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